REPORT

Determination according to EN 13381-4:2013 of the contribution to the fire resistance of structural steel members by a three or four sided single layer boxed protection from PROMATECT®-200 boards Assessment report numerical regression

Report no.
2013-Efectis-RO344e
Prompt Research and Technology Centre N.V. Bormstratat 2.4 B-2830 Tisselt Belgium

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Project number
Date of issue
Number of pages



2013344
September 2013
L.M. Noordijk, M.SC.


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1. SUBJECT

PROMATECT®-200, a fire resistant board material
2. INVESTIGATION

Contribution, according to EN 13381-4:2013, to the fire resistance of strastural skeel members by a single layer three or four sided boxed protection from PROMATECT®-200 boards. The method for processing the results is the numerical regression assessment method.

### 3.1 SPONSOR

Promat Research and Technology Centre N.V. Bormstraat 24 B-2830 Tisselt Belgium

### 3.2 MANUFACTURER

Promat Research and Technology Centre M.V
Bormstraat 24
B-2830 Tisselt
Belgium
4. LOCATION AND DATES OF THE INVESTIGATIONS

9 unloaded short columns

- Laboratory: TNø Centre for Fire Research, Rijswijk, The Netherlands;
- Test dates: 23 and 30 August and 6 September 2001;
- TNO Report: 2001-CVB-RO4661.

1 unloaded short column

- Laboratory: Efectis Nederland BV, Rijswijk, The Netherlands;
- Test dates: 30 November 2011;
- Efectis Report: 2011-Efectis-R0694

3 unloaded short cotumns
Waboratory: Efectis Nederland BV, Rijswijk, The Netherlands;
Test dates: 7 March 2012;

- Efectis Report: 2012-Efectis-R0223.

2 loaded beams and 4 unloaded short columns

- Laboratory: Efectis Nederland BV, Rijswijk, The Netherlands;
- $\quad$ Test dates: 13-3-2013 ( 15 mm beam test) and 23-5-2013 ( 30 mm beam test and 4 unloaded columns)
Efectis Report: 2013-Efectis-R0188 and 2013-Efectis-R0228


## 5. TEST SPECIMENS

For a description of the test specimens and the method of application of the boards we refer to the test reports mentioned in the table below. A summary of the test specimens used for the assessment according to EN 13381-4:2013 (numerical regression method) is given in the table below.

### 5.1 TEST SPECIMENS



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### 5.2 DIMENSIONS OF THE TEST SPECIMENS

| Type | Protection <br> thickness | Height | Width | Thickness <br> flange | Thickness <br> web | Area | Perimeter | Actual <br> section <br> factor |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | mm | mm | mm | mm | mm | m 2 | m | $\mathrm{~m}-1$ |
| HEM 280 | 15 | 308 | 285 | 32.7 | 17.8 | 0.02293056 | 1.186 | 52 |
| HEM 280 | 20 | 310 | 190 | 32.4 | 19.2 | 0.01700276 | 1 | 59 |
| HEM 280 | 25 | 310 | 287 | 32.7 | 19.1 | 0.023442 | 1.194 | 51 |
| HEA 200 | 15 | 199 | 195 | 10.0 | 7.1 | 0.00515211 | 0.788 | 153 |
| HEA 200 | 25 | 200 | 196 | 10.0 | 7.2 | 0.00519712 | 0.792 | 152 |
| HEA 200 | 30 | 191 | 201 | 10.2 | 6.7 | 0.005243 | 0.784 | 150 |
| IPE 200 | 15 | 203 | 100 | 8.8 | 5.7 | 0.00281678 | 0.606 | 215 |
| IPE 200 | 20 | 200 | 100 | 89 | 5.5 | 0.00277265 | 0.6 | 216 |
| IPE 200 | 25 | 200 | 100 | 8.8 | 5.4 | 0.00274496 | 0.6 | 219 |
| IPE 200 | 30 | 202 | 102 | 7.9 | 5.7 | 0.002673 | 0.608 | 227 |
| IPE 80 | 20 | 80 | 47 | 5.4 | 4.2 | 0.0008017 | 0.254 | 317 |
| IPE 80 | 25 | 83 | 47 | 6.4 | 4.1 | 0.000797425 | 0.254 | 319 |
| IPE 80 | 30 | 80 | 45 | 4.8 | 4.2 | 0.000728 | 0.25 | 344 |



5.3 CORRECTED TIMES

| $\begin{gathered} \mathrm{Pi} \\ \mathrm{~m}-1 \\ \hline \end{gathered}$ | 52 | $59$ | $5$ | 153 | 152 | 150 | 215 | 216 | 219 | 227 | 317 | 319 | 344 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \hline \text { DFT } \\ & \mathrm{mm} \end{aligned}$ | 15 | $201$ | $25$ | $\geq 15$ | 25 | 30 | 15 | 20 | 25 | 30 | 20 | 25 | 30 |
| Temp ${ }^{\circ} \mathrm{C}$ | Time [min.] | Tinme [min.] | Time [min. 1 | Time [min.] | Time <br> [min.] | Time [min.] | Time [min.] | Time [min.] | Time [min.] | Time [min.] | Time [min.] | Time [min.] | Time [min.] |
| 350 | 69.15 | 103.96 | 130.84 | 38.45 | 57.06 | 83.75 | 35.05 | 45.72 | 47.02 | 76.63 | 38.67 | 41.32 | 63.26 |
| 400 | 78.02 | 118.94 | 148.95 | 42.68 | 63.82 | 91.56 | 38.54 | 50.08 | 51.73 | 82.57 | 41.82 | 44.52 | 66.8 |
| 450 | 87.45 | 134.93 | 169.16 | 47.88 | 71.36 | 100.48 | 42.2 | 54.85 | 56.99 | 89.54 | 45.36 | 48.13 | 71.07 |
| 500 | 98.44 | 151.7 | 191.5 | 52.35 | 79.92 | 110.94 | 46.23 | 60.19 | 62.76 | 97.91 | 49.45 | 52.34 | 76.34 |
| 550 | 104.73 | 168.92 | 215.82 | 57.67 | 89.61 | 123.2 | \$0.6 | 66.26 | 69.35 | 107.69 | 54.2 | 57.26 | 82.51 |
| 600 | 116.24 | 183.39 | 236.85 | 63.36 | 99.79 | 133.95 | 55.6 | 73.34 | 76.32 | 115.88 | 59.35 | 62.4 | 87.16 |
| 650 | 125.65 | 201.23 | 258.34 | 69.5 | 111.97 | 148.33 | 61.27 | 81.81 | 84.19 | 127.42 | 65.45 | 68.61 | 93.85 |
| 700 | 135.69 | 218.83 | 275.94 | 75.97 | 126.09 | 164.04 | $67.45$ | 92,1 | 92.33 | 140.62 | 72.48 | 75.95 | 101.39 |
| 750 | 142.05 | 237.04 | 293.44 | 82.76 | 145.79 | 182.84 | 74.92 | $105 / 32$ | 103.34 | $158.54$ | 81.52 | 84.8 | 110.9 |

6. ASSESSMENT OF RESULTS

### 6.1 CORRECTION OF THE TIMES TO REACH CERTAIN STEEL TEMPERATURES OF THE COLUMNS (MECHANICAL BEHAVIOUR)

From the measured steel temperatures of the loaded beams en the unloaded reference beams characteristic temperatures were determined according to par. 3.1.11 in EN 13381-4:2013.
With the times to reach certain characteristic temperatures correction factors were determined. In agreement with Annex D of EN 13381-4:2013, the correction temperatures above the characteristic temperature at which failure of the toaded section occurred, the minimum observed correction factor just before failure is used. The temperature correction factors for single layer Promatect-200 boards are given in ffgure 6.1.)


Figure 6.1 temperature coryection factors for both beam tests.
These correction factors were, according to EN 13381-4:2013, applied to the times to reach certain average temperatures in the columns.

### 6.2 DETERMINATION OF THE EFFECTIVE HEAT CONDUCTIVITY COEFFICIENT (THERMAL BEHAVIOUR)

According to EN 13381-4:2013 the effective heat conductivity coefficient was determined with the following formula.
$t=a_{0}+a_{1} d_{p}+a_{2} \frac{d_{p}}{A_{m} / V}+a_{3} \theta_{a}+a_{4} d_{p} \theta_{a}+a_{5} d_{p} \frac{\theta_{a}}{A_{m} / V}+a_{6} \frac{\theta_{a}}{A_{m} / V}+a_{7} \frac{1}{A_{m} / V}$

Wherein:
$t$ minutes
$d_{p}$
$A_{m} / V$
$a_{0} t / m a_{7}$
$\theta_{a}$
is the corrected time to reach design temperature $\theta_{a}$ in is the board thickness in mm is de measured section factor in $\mathrm{m}^{-1}$ are constants is the critical steel temperature in


The constants $\mathrm{a}_{0} \mathrm{t} / \mathrm{m} \mathrm{a}_{7}$ are determined using linear regression techniques following the criteria of EN 13381-4 :2010:
a) For each short section the predicted time to reath the design temperature shall not exceed the corrected time by more than $15 \%$
b) The mean value of all percentage differences as catculated in a) shall be less than zero
c) A maximum of $30 \%$ of all individual vatues of all percentage differences as calculated in a) shall be more than zero

The results of the calculation are:

$t=-27.301+1.478086 \times d_{p}+(-202.249) \times \frac{d_{p}}{d_{m}}+0.068536 \times \theta_{a}+(-0.00018) \times d_{p} \theta_{a}+$
$1.188467 \times d_{p} \frac{\theta_{a}}{A_{m} / V}+\left(-11.1377 \times \times \frac{\theta_{a}}{A_{m} / V}+3467.681 \times \frac{1}{A_{m} / V}\right.$

### 6.3 GRAPHS

Based on the effective heat conductivity coefficient two sets of data were calculated:

- Graphs in Figure to. Tto 10.9 in which for a specific design steel temperature ( 350 to $750^{\circ} \mathrm{C}$ in stens of $50^{\circ} \mathrm{C}$ ) the relation between the fire resistance and the section factor is given fora certain protected structural steel member.
- Tables in chapter 11 which give the required thickness for a certain fire resistance (in minutes) for a given critical steel temperature and section factor.


The fire resistance of structural steel members protected with a single layer three or foursided boxed protection from PROMATECT®-200 may according to EN 13381-4:2013 be determined using figures $10.1 \mathrm{t} / \mathrm{m} 10.9$ and the tables in chapter 11 under the conditions given in chapter 8 of this report.

## 8. CONDITIONS AND FIELD OF APPLICATION

The section factor has to be determined according to figure 1 of EN 13381-4:2013.
The figures 10.1 to 10.9 and the tables in chapter 11 are only valid under the conditions

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mentioned below:

- $46 \mathrm{~m}-1 \leq \mathrm{Am} / \mathrm{V} \leq 378 \mathrm{~m}-1$ (section factor)
- $14.25 \leq \mathrm{dp} \leq 31.5 \mathrm{~mm}$ (thickness)
- $350^{\circ} \mathrm{C} \leq \theta \mathrm{a} \leq 750^{\circ} \mathrm{C}$

If the figures in chapter 10 or the tables in chapter 11 are used, intermediate values for the critical steel temperature may be interpolated using linear interpolation.
The results in chapter 10 and 11 are valid for three and four sided boxed pretection.

P.W.M. Kortekaas

Project Leader Resistant to Fire


9. MEASURED CORRECTED TIMES VS. CALCULATED TIMES

| Critical steel temp ${ }^{\circ} \mathrm{C}$ | Thickness mm | Section factor m-1 | Tmeas Min. | Tcalc Min. | Tcalc/Tmeas |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 350 | 15 | 52 | 69.15 | 70.71 | 1.023 |
| 350 | 20 | 59 | 103.96 | 89.46 | 0.861 |
| 350 | 25 | 51 | 130.34 | 127.41 | 0.978 |
| 350 | 15 | 153 | 38.45 | 35.86 | 0.933 |
| 350 | 25 | 152 | 68.5 | 64.06 | 0.935 |
| 350 | 30 | 150 | 83.75 | 78.62 | 0.939 |
| 350 | 15 | 215 | 35.05 | 30.69 | 0.875 |
| 350 | 20 | 216 | 47.02 | 42.6 | 0.906 |
| 350 | 25 | 219 | 61.85 | 54.27 | 0.877 |
| 350 | 30 | 227 | 76.63 | 65.23 | 0.851 |
| 350 | 20 | 317 | 41.32 | 36.99 | 0.895 |
| 350 | 25 | 319 | 48.47 | 47.31 | 0.976 |
| 350 | 30 | 344 | 63.26 | (56.36 | ) 0.891 |
| 400 | 15 | 52 | 78.02 | 80.43 | 1.031 |
| 400 | 20 | 59 | 118.94 | 103.42 | 0.869 |
| 400 | 25 | 51 | 148.95 | 14882 | 0.999 |
| 400 | 15 | 153 | 42.68 | 41.34 | 0.969 |
| 400 | 25 | 152 | 45.42 | 73.37 | 0.973 |
| 400 | 30 | 150 | 91.56 | 89.95 | 0.982 |
| 400 | 15 | 215 | 38.54 | 35.53 | 0.922 |
| 400 | 20 | 216 | 51.73 | 48.78 | 0.943 |
| 400 | 25 | 219 | 67). 57 | 61.72 | 0.913 |
| 400 | 30 | 227 | 82.57 | 73.79 | 0.894 |
| 400 | 20 | 317 | 44.52 | 42.23 | 0.949 |
| 400 | 25 | 319 | 51.62 | 53.43 | 1.035 |
| 400 | $30 \sqrt{ }$ | 344 | 66.8 | 63.08 | 0.944 |
| 450 | 15 | 52 | 87.45 | 90.16 | 1.031 |
| 450 | 20 | 59 | 134.93 | 117.37 | 0.87 |
| 450 | $\sqrt{25}$ | - 51 | 169.16 | 170.24 | 1.006 |
| 450 | 15 | 153 | 47.38 | 46.82 | 0.988 |
| 450 | 25 | 152 | 83.13 | 82.69 | 0.995 |
| 450 | 30 | 150 | 100.48 | 101.28 | 1.008 |
| 450 | 15 | 215 | 42.2 | 40.38 | 0.957 |
| 450 | 20 | 216 | 56.99 | 54.95 | 0.964 |
| 450 | 25 | 219 | 74.09 | 69.16 | 0.933 |
| 450 | 30 | 227 | 89.54 | 82.35 | 0.92 |
| 450 | 20 | 317 | 48.13 | 47.47 | 0.986 |
| 450 | 25 | 319 | 55.2 | 59.54 | 1.079 |



10. DESIGN GRAPHS

Figure 10.1 : Fire resistance as function of the section factor and the board thickness for a critical steel temperature of $350^{\circ} \mathrm{C}$.

Figure 10.2

Figure 10.3

Figure 10.4

Figure 10.5 : Fire resistance as function of the section factor and the board thickness for a critical steel temperature of $550^{\circ} \mathrm{C}$.

Figure 10.6 : Fire resistance as function of the section factor and the board thickness for a critical steet temperature of $600^{\circ} \mathrm{C}$.

Figure 10.7 : Fire resistance as function of the section factor and the board thickness for a critical stee temperature of $650^{\circ} \mathrm{C}$.

Figure 10.8 : Fire resistance as function or the section factor and the board thickness for a critical steel temperature of $700^{\circ} \mathrm{C}$.

Figure 10.9 : Fire resistance as function of the section factor and the board thickness for a critical steel temperature of $750^{\circ} \mathrm{C}$.


[^0]The European experts in fire safety

Figure 10.1 : critical steel temperature $350^{\circ} \mathrm{C}$
(

[^1]
Figure 10.3 : critical steel temperature $450^{\circ} \mathrm{C}$


[^2]Efectis Nederland Report
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Figure 10.6 : critical steel temperature $600^{\circ} \mathrm{C}$
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Figure 10.7 : critical steel temperature $650^{\circ} \mathrm{C}$


[^3](

[^4]$\qquad$
11. DESIGN TABLES

Design table 1 : fire resistance 30 minutes required protection thickness in mm

| Section factor m-1 | Critical steel temperature ${ }^{\circ} \mathrm{C}$ |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 350 | 400 | 450 | 500 | 550 |  | 659 | 700 | 750 |
| 0 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 |
| 45.9 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 |
| 50 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 |
| 60 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 |
| 70 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 |
| 80 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 |
| 90 | 14.2 | 14.2 | 14.2 | 14.2 | 142 | 14.2 | 14.2 | 14.2 | 14.2 |
| 100 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 |
| 110 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 |
| 120 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 |
| 130 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 |
| 140 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 |
| 150 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 |
| 160 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 |
| 170 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 |
| 180 | 14.2 | 14.2 | 14.8 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 |
| 190 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 |
| 200 | 14.3 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 |
| 210 | 14.6 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 |
| 220 | 14.8 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 |
| 230 | 15.1 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 |
| 240 | 15.3 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 |
| 250 | 15.5 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 |
| 260 | 15.7 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 |
| 270 | 15.9 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 |
| 280 |  | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 |
| 290 | 16.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 |
| 300 | $\sqrt{6.4}$ | 14.4 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 |
| 310 | 16.5 | 14.5 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 |
| 320 | 16.7 | 14.6 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 |
| 330 | 16.8 | 14.8 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 |
| 340 | 17 | 14.9 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 |
| 350 | 17.1 | 15 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 |
| 360 | 17.2 | 15.1 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 |
| 370 | 17.3 | 15.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 |
| 378.4 | 17.4 | 15.3 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 |

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Design table 2 : fire resistance 60 minutes required protection thickness in mm

| Section factor m-1 | Critical steel temperature ${ }^{\circ} \mathrm{C}$ |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 350 | 400 | 450 | 500 | 550 | 600 | 650 | 700 | 750 |
| 0 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 44.2 | 14.2 | 14.2 | 14.2 |
| 45.9 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 |
| 50 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 44.2 | 14.2 | 14.2 | 14.2 |
| 60 | 14.3 | 14.2 | 14.2 | 14.2 | 14.2 | (14.2 | 14.2 | 14.2 | 14.2 |
| 70 | 15.6 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 |
| 80 | 16.9 | 15.1 | 14.2 | 14.2 | 14.2 | +14,2 | 14.2 | 14.2 | 14.2 |
| 90 | 18.1 | 16 | 14.5 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 |
| 100 | 19.1 | 16.9 | 15.3 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 |
| 110 | 20.1 | 17.8 | 16 | 14.6 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 |
| 120 | 21 | 18.6 | 16.7 | 15.2 | 14.2 | J14.2 | 14.2 | 14.2 | 14.2 |
| 130 | 21.9 | 19.3 | 17.3 | 15.8 | 14.5 | 14.2 | 14.2 | 14.2 | 14.2 |
| 140 | 22.7 | 20 | 18 | 163 | 14.9 | 14.2 | 14.2 | 14.2 | 14.2 |
| 150 | 23.4 | 20.7 | 18.5 | 16.8 | 15.4 | 14.2 | 14.2 | 14.2 | 14.2 |
| 160 | 24.1 | 21.3 | 19.1 | 17.3 | 15.8 | 14.6 | 14.2 | 14.2 | 14.2 |
| 170 | 24.7 | 21.9 | 19.6 | (178) | 16.2 | 14.9 | 14.2 | 14.2 | 14.2 |
| 180 | 25.4 | 22.4 | 20.1 | 18.2 | 16.6 | 15.3 | 14.2 | 14.2 | 14.2 |
| 190 | 25.9 | 23 | 20.6 | 18.6 | 17 | 15.6 | 14.4 | 14.2 | 14.2 |
| 200 | 26.5 | 23.5 | 24 | 19 | 17.3 | 15.9 | 14.7 | 14.2 | 14.2 |
| 210 | 27 | 23.9 | 21.5 | 19.4 | 17.7 | 16.2 | 14.9 | 14.2 | 14.2 |
| 220 | 27.5 | 24.4 | 21.9 | 19.8 | 18 | 16.5 | 15.2 | 14.2 | 14.2 |
| 230 | 27.9 | 24.8 | 22.3 | 20.2 | 18.3 | 16.8 | 15.4 | 14.2 | 14.2 |
| 240 | 28.3 | 25.2 | 22.7 | 20.5 | 18.7 | 17.1 | 15.7 | 14.5 | 14.2 |
| 250 | 28.7 | 25/6 | 23 | 20.8 | 19 | 17.3 | 15.9 | 14.7 | 14.2 |
| 260 | 29.1 | 26 | 23.4 | 21.2 | 19.3 | 17.6 | 16.1 | 14.9 | 14.2 |
| 270 | 29.5 | 26.4 | 23.7 | 21.5 | 19.5 | 17.8 | 16.4 | 15.1 | 14.2 |
| 280 | 29.9 | 26.7 | 24 | 21.8 | 19.8 | 18.1 | 16.6 | 15.2 | 14.2 |
| 290 | 30.2 | 27 | 24.4 | 22.1 | 20.1 | 18.3 | 16.8 | 15.4 | 14.2 |
| 300 | 30.5 | 27.4 | 24.7 | 22.3 | 20.3 | 18.6 | 17 | 15.6 | 14.4 |
| 310 | 30.8 | 27.7 | 24.9 | 22.6 | 20.6 | 18.8 | 17.2 | 15.8 | 14.5 |
| 320 | 31.1 | 27.9 | 25.2 | 22.9 | 20.8 | 19 | 17.4 | 15.9 | 14.7 |
| 330 | (31.4 | 28.2 | 25.5 | 23.1 | 21 | 19.2 | 17.6 | 16.1 | 14.8 |
| 340 | - | 28.5 | 25.7 | 23.4 | 21.3 | 19.4 | 17.8 | 16.3 | 14.9 |
| 350 |  | 28.8 | 26 | 23.6 | 21.5 | 19.6 | 17.9 | 16.4 | 15.1 |
| 360 | - | 29 | 26.2 | 23.8 | 21.7 | 19.8 | 18.1 | 16.6 | 15.2 |
| 370 | - | 29.2 | 26.5 | 24 | 21.9 | 20 | 18.3 | 16.7 | 15.3 |
| 378.4 | - | 29.4 | 26.7 | 24.2 | 22.1 | 20.1 | 18.4 | 16.9 | 15.4 |

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Design table 3 : fire resistance 90 minutes required protection thickness in mm

| Section <br> factor <br> $\mathrm{m}-1$ | 350 | 400 | 450 | 500 | 550 | 600 | 650 | 700 | 750 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 17 | 15.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 |
| 45.9 | 17 | 15.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 |
| 50 | 18 | 16.1 | 14.7 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 |
| 60 | 20.3 | 17.9 | 16.2 | 15 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 |
| 70 | 22.4 | 19.7 | 17.7 | 16.2 | 15.1 | 14.2 | 14.2 | 14.2 | 14.2 |
| 80 | 24.3 | 21.3 | 19.1 | 17.5 | 16.1 | 15.1 | 14.2 | 14.2 | 14.2 |
| 90 | 26 | 22.8 | 20.4 | 18.6 | 17.1 | 15.9 | 14.9 | 14.2 | 14.2 |
| 100 | 27.6 | 24.2 | 21.7 | 19.7 | 18.1 | 16.8 | 15.7 | 14.8 | 14.2 |
| 110 | 29.1 | 25.5 | 22.8 | 20.7 | 19 | 17 | 6 | 16.4 | 15.4 |
| 120 | 30.5 | 26.8 | 23.9 | 21.7 | 29.9 | 18.4 | 17.1 | 16 | 15.5 |
| 130 | - | 27.9 | 25 | 22.6 | 20.7 | 19.1 | 17.8 | 16.6 | 15.6 |
| 140 | - | 29 | 25.9 | 23.5 | 21.5 | 19.8 | 18.4 | 17.2 | 16.1 |
| 150 | - | 30 | 26.9 | 24.3 | 22.2 | 20.5 | 19 | 17.7 | 16.6 |
| 160 | - | 31 | 27.8 | 25.1 | 23 | 21.2 | 19.6 | 18.3 | 17.1 |
| 170 | - | - | 28.6 | 25.9 | 23.7 | 21.8 | 20.2 | 18.8 | 17.6 |
| 180 | - | - | 29.4 | 26.6 | 24.4 | 22.4 | 20.7 | 19.3 | 18 |
| 190 | - | - | 30.2 | 27.3 | 25 | 23 | 21.3 | 19.8 | 18.5 |
| 200 | - | - | 30.9 | 28 | 25.6 | 23.6 | 21.8 | 20.3 | 18.9 |
| 210 | - | - | - | 28.3 | 26.2 | 24.1 | 22.3 | 20.7 | 19.3 |
| 220 | - | - | - | 29.3 | 26.8 | 24.7 | 22.8 | 21.2 | 19.7 |
| 230 | - | - | - | 29.9 | 27.4 | 25.2 | 23.3 | 21.6 | 20.1 |
| 240 | - | - | - | 30.5 | 27.9 | 25.7 | 23.7 | 22 | 20.5 |
| 250 | - | - | - | 31 | 28.4 | 26.1 | 24.2 | 22.4 | 20.9 |
| 260 | - | - | - | - | 28.9 | 26.6 | 24.6 | 22.8 | 21.2 |
| 270 | - | - | - | - | 29.4 | 27.1 | 25 | 23.2 | 21.6 |
| 280 | - | - | - | - | 29.9 | 27.5 | 25.4 | 23.6 | 21.9 |
| 290 | - | - | - | - | 30.3 | 27.9 | 25.8 | 24 | 22.3 |
| 300 | - | - | - | - | 30.7 | 28.3 | 26.2 | 24.3 | 22.6 |
| 310 | - | - | - | - | 31.2 | 28.7 | 26.6 | 24.7 | 22.9 |
| 320 | - | - | - | - | - | 29.1 | 26.9 | 25 | 23.3 |
| 330 | - | - | - | - | - | 29.5 | 27.3 | 25.3 | 23.6 |
| 340 | - | - | - | - | - | 29.9 | 27.6 | 25.7 | 23.9 |
| 350 | - | - | - | - | - | 30.2 | 28 | 26 | 24.2 |
| 360 | - | - | - | - | - | 30.6 | 28.3 | 26.3 | 24.4 |
| 370 | - | - | - | - | - | 30.9 | 28.6 | 26.6 | 24.7 |
| 378.4 | - | - | - | - | - | 31.2 | 28.9 | 26.8 | 24.9 |
|  |  |  |  |  |  |  |  |  |  |

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Design table 4 : fire resistance 120 minutes required protection thickness in mm

| Section factor m-1 | Critical steel temperature ${ }^{\circ} \mathrm{C}$ |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 350 | 400 | 450 | 500 | 550 | 600 | 650 | 700 | 750 |
| 0 | 22 | 19.3 | 17.5 | 16.1 | 15 | 14.2 | 14.2 | 14.2 | 14.2 |
| 45.9 | 22 | 19.3 | 17.5 | 16.1 | 15 | 14.2 | 14.2 | 14.2 | 14.2 |
| 50 | 23.3 | 20.5 | 18.4 | 16.9 | 15.7 | 14.8 | 14.2 | 14.2 | 14.2 |
| 60 | 26.4 | 23 | 20.6 | 18.8 | 17.4 | 16.2 | 15.3 | 14.5 | 14.2 |
| 70 | 29.2 | 25.4 | 22.6 | 20.6 | 18.9 | 17.6 | 16.5 | 15.6 | 14.8 |
| 80 | - | 27.6 | 24.6 | 22.2 | 20.4 | 18.9 | 17.7 | 16.7 | 15.8 |
| 90 | - | 29.6 | 26.4 | 23.8 | 21.8 | 20.2 | 18.8 | 17.7 | 16.7 |
| 100 | - | - | 28.1 | 25.3 | 23.2 | 21.4 | 19.9 | 18.7 | 17.6 |
| 110 | - | - | 29.6 | 26.8 | -24.5 | 22.0 | 21 | 19.6 | 18.5 |
| 120 | - | - | 31.2 | 28.1 | <25.7 | 23.7 | 22 | 20.6 | 19.3 |
| 130 | - | - | - | 29.4 | $\underline{26.9}$ | 24.8 | 23 | 21.5 | 20.1 |
| 140 | - | - | - | 30.7 | 28 | 25.8 | 23.9 | 22.3 | 20.9 |
| 150 | - | - | - | - | 29.) | 26.8 | 24.8 | 23.2 | 21.7 |
| 160 | - | - | - |  | 30,1 | 27.8 | 25.7 | 24 | 22.4 |
| 170 | - | - | - | - | $\triangle 31.1$ | 28.7 | 26.6 | 24.7 | 23.1 |
| 180 | - | - | - | , | ) | 29.6 | 27.4 | 25.5 | 23.8 |
| 190 | - | - |  | - | - | 30.4 | 28.2 | 26.2 | 24.5 |
| 200 | - | - |  |  | - | 31.2 | 28.9 | 26.9 | 25.2 |
| 210 | - | - |  | $\rightarrow$ | - | - | 29.7 | 27.6 | 25.8 |
| 220 | - | - |  |  | - | - | 30.4 | 28.3 | 26.4 |
| 230 | - | - |  | - | - | - | 31.1 | 28.9 | 27 |
| 240 | - | - | - | - | - | - | - | 29.6 | 27.6 |
| 250 | - |  |  | - | - | - | - | 30.2 | 28.2 |
| 260 | - |  | - | - | - | - | - | 30.8 | 28.8 |
| 270 | - |  | -) | - | - | - | - | 31.4 | 29.3 |
| 280 | - |  | . | - | - | - | - | - | 29.8 |
| 290 | - |  | $>$ | - | - | - | - | - | 30.4 |
| 300 |  | - | - | - | - | - | - | - | 30.9 |
| 310 |  | - | - | - | - | - | - | - | 31.4 |



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Design table 5 : fire resistance 150 minutes required protection thickness in mm

| Section <br> factor <br> $\mathrm{m}-1$ | Critical steel temperatures ${ }^{\circ} \mathrm{C}$ |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 350 | 400 | 450 | 500 | 550 | 600 | 650 | 700 | 750 |  |  |
| 0 | 27 | 23.4 | 20.9 | 19.1 | 17.7 | 16.6 | 15.6 | 14.9 | 14.2 |  |  |
| 45.9 | 27 | 23.4 | 20.9 | 19.1 | 17.7 | 16.6 | 15.6 | 14.9 | 14.2 |  |  |
| 50 | 28.7 | 24.8 | 22.1 | 20.1 | 18.6 | 17.4 | 16.4 | 15.5 | 14.8 |  |  |
| 60 | - | 28.1 | 24.9 | 22.6 | 20.7 | 19.3 | 18.1 | 17.1 | 16.2 |  |  |
| 70 | - | 31.1 | 27.5 | 24.9 | 22.8 | 21.1 | 19.7 | 18.5 | 17.5 |  |  |
| 80 | - | - | 30 | 27 | 24.7 | 22.8 | 21.3 | 19.9 | 18.8 |  |  |
| 90 | - | - | - | 29.1 | 26.5 | 24.5 | 22.8 | 21.3 | 20.1 |  |  |
| 100 | - | - | - | 31 | 28.3 | 26.1 | 24.2 | 22.6 | 21.3 |  |  |
| 110 | - | - | - | - | 30 | 27.6 | 25.6 | 23.9 | 22.4 |  |  |
| 120 | - | - | - | - | 2 | - | 29 | 26.9 | 25.1 |  |  |
| 130 | - | - | - | - | - | 30.5 | 28.2 | 26.3 | 24.7 |  |  |
| 140 | - | - | - | - | - | - | 29.5 | 27.5 | 25.7 |  |  |
| 150 | - | - | - |  | - | - | 30.7 | 28.6 | 26.8 |  |  |
| 160 | - | - | - | - | - | - | - | 29.6 | 27.7 |  |  |
| 170 | - | - | - | - | - | - | - | 30.7 | 28.7 |  |  |
| 180 | - | - | - | - | - | - | - | - | 29.7 |  |  |
| 190 | - | - | - | - | - | - | - | - | 30.6 |  |  |
| 200 | - | - | - | - | - | - | - | - | 31.5 |  |  |

Design table 6 : fire resistance 180 minutes requiked protection thickness in mm

| Section factor m-1 | Critical steel temperature ${ }^{\circ} \mathrm{C}$ |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 350 | 400 | 450 | 500 | 550 | 600 | 650 | 700 | 750 |
| 0 | - | 27.5 | 24.4 | 22.1 | 20.4 | 19 | 17.8 | 16.9 | 16.1 |
| 45.9 | - | 27.5 | 24.4 | 22.1 | 20.4 | 19 | 17.8 | 16.9 | 16.1 |
| 50 | - | 29.2 | -25.9 | 23.4 | 21.5 | 20 | 18.7 | 17.7 | 16.8 |
| 60 | - | - | 29.3 | 26.4 | 24.1 | 22.3 | 20.8 | 19.6 | 18.5 |
| 70 | - | - | - | 29.2 | 26.6 | 24.6 | 22.9 | 21.4 | 20.2 |
| 80 |  | $\bigcirc$ | - | - | 29 | 26.7 | 24.8 | 23.2 | 21.8 |
| 90 |  |  | - | - | 31.3 | 28.7 | 26.7 | 24.9 | 23.4 |
| 100 | - | $\cdots$ | - | - | - | 30.7 | 28.5 | 26.6 | 24.9 |
| 110 | - | - | - | - | - | - | 30.2 | 28.1 | 26.4 |
| 120 | , | ) | - | - | - | - | - | 29.7 | 27.8 |
| 130 |  | - | - | - | - | - | - | 31.2 | 29.2 |
| 140 | - | - | - | - | - | - | - | - | 30.5 |

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Design table 7 : fire resistance 210 minutes required protection thickness in mm

| Section factor m-1 | Critical steel temperature ${ }^{\circ} \mathrm{C}$ |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 350 | 400 | 450 | 500 | 550 | 600 | 650 | 700 | 750 |
| 0 | - | - | 27.9 | 25.2 | 23.1 | 21.4 | 20 | 18.9 | 17.9 |
| 45.9 | - | - | 27.9 | 25.2 | 23.1 | 21.4 | 20 | 18.9 | 17.9 |
| 50 | - | - | 29.6 | 26.7 | 24.4 | 22.6 | 27.1 | 19.8 | 18.8 |
| 60 | - | - | . | 30.2 | 27.5 | 25.4 | 23.6 | 22.1 | 20.9 |
| 70 | - | - | - | - | 30.5 | 28 | 26 | 24.3 | 22.9 |
| 80 | - | - | - | - |  | 30,6 | 28.3 | 26.5 | 24.9 |
| 90 | - | - | - | - |  | ) | 30.6 | 28.5 | 26.8 |
| 100 | - | - | - | - |  | ) | - | 30.5 | 28.6 |
| 110 | - | - | - |  |  |  | - | - | 30.3 |

Design table 8 : fire resistance 240 minutes required protection thickness in mm

| Section factor m-1 | Critical steel temperature ${ }^{\circ} \mathrm{C}$ |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 350 | 400 | 450 | 500 |  | 600 | 650 | 700 | 750 |
| 0 | - | - | 31.4 | 28.2 | 25.7 | 23.8 | 22.2 | 20.9 | 19.8 |
| 45.9 | - | - | 31.4 | 28.2 | 25.7 | 23.8 | 22.2 | 20.9 | 19.8 |
| 50 | - | - |  | 29.9 | 27.3 | 25.2 | 23.4 | 22 | 20.8 |
| 60 | - | - |  |  | 30.9 | 28.4 | 26.4 | 24.7 | 23.2 |
| 70 | - | - |  | $\xrightarrow{-}$ | - | - | 29.2 | 27.2 | 25.6 |
| 80 | - | - | - |  | - | - | - | 29.7 | 27.9 |
| 90 | - | - |  | - | - | - | - | - | 30.1 |

Design table 9 : fire resistance 270 minutes required protection thickness in mm


Design table 10 :fireresistance 300 minutes required protection thickness in mm

| Section <br> factor <br> $\mathrm{m}-1$ | Critical steel temperature ${ }^{\circ} \mathrm{C}$ |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 350 | 400 | 450 | 500 | 550 | 600 | 650 | 700 | 750 |  |
| 0 | - | - | - | - | 31.1 | 28.6 | 26.6 | 24.9 | 23.4 |  |
| 45.9 | - | - | - | - | 31.1 | 28.6 | 26.6 | 24.9 | 23.4 |  |
| 50 | - | - | - | - | - | 30.4 | 28.1 | 26.3 | 24.8 |  |
| 60 | - | - | - | - | - | - | - | 29.8 | 27.9 |  |

Design table 11 : fire resistance 330 minutes required protection thickness in mm

| Section <br> factor <br> $\mathrm{m}-1$ | Critical steel temperature ${ }^{\circ} \mathrm{C}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 350 | 400 | 450 | 500 | 550 | 600 | 650 | 700 | 750 |  |  |  |  |  |
| 0 | - | - | - | - | - | 31 | 28.7 | 26.9 | 25.3 |  |  |  |  |  |
| 45.9 | - | - | - | - | - | 31 | 28.7 | 26.9 | 25.3 |  |  |  |  |  |
| 50 | - | - | - | - | - | - | 30.5 | 28.5 | 26.8 |  |  |  |  |  |
| 60 | - | - | - | - | - | - | - | - | 30.3 |  |  |  |  |  |

Design table 12 : fire resistance 360 minutes required protection thickness in mm

| Section factor m-1 | Critical stea/ temperature ${ }^{\circ} \mathrm{C}$ |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 350 | 400 | 450 | 500 | $z_{550}$ | $\bigcirc 600$ | 650 | 700 | 750 |
| 0 | - | - | - | - |  | - | 30.9 | 28.9 | 27.1 |
| 45.9 | - | - | - | $\triangle$ | - | - | 30.9 | 28.9 | 27.1 |
| 50 | - | - | - |  | - | - | - | 30.6 | 28.7 |





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[^1]:    Figure 10.2 : critical steel temperature $400^{\circ} \mathrm{C}$

[^2]:    Figure 10.4 : critical steel tomperat $500^{\circ} \mathrm{C}$

[^3]:    Figure 10.8 : critical steel temperature $700^{\circ} \mathrm{C}$

[^4]:    Figure 10.9 : critical steel temperature $750^{\circ} \mathrm{C}$

